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1 How to Read this Design Guide

This Design Guide will introduce all aspects of the Advanced Harmonic Filters for your VLT® FC Series Drive. It describes Harmonics and how to mitigate them, provide installation instructions and guidance about how to programme the frequency converter.

Danfoss technical literature is also available online at www.danfoss.com/BusinessAreas/DrivesSolutions/Documentations/Technical+Documentation.



2 Safety and Conformity

2.1.1 Symbols

Symbols used in this manual:

NOTE

Indicates something to be noted by the reader.



CAUTION

Indicates a general warning.



WARNING

Indicates a high-voltage warning.

★ Indicates default setting

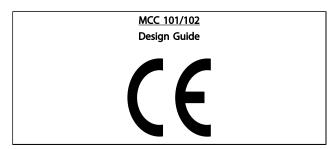
2.1.2 Abbreviations

Active Power	Р
Advanced Harmonic Filter	AHF
Alternating current	AC
American wire gauge	AWG
Ampere/AMP	А
Apparent Power	S
Degrees Celsius	°C
Direct current	DC
Displacement Power Factor	DPF
Electro Magnetic Compatibility	EMC
Drive	FC
Gram	g
Harmonic Calculation Software	HCS
Hertz	Hz
Kilohertz	kHz
Local Control Panel	LCP
Meter	m
Millihenry Inductance	mH
Milliampere	mA
Millisecond	ms
Minute	min
Motion Control Tool	мст
Nanofarad	nF
Newton Meters	Nm
Nominal motor current	I _{M,N}
Nominal motor frequency	f _{M,N}
Nominal motor power	P _{M,N}
Nominal motor voltage	U _{M,N}
Parameter	par.
Partial Weighted Harmonic Distor-	PWHD
tion	
Point of Common Coupling	PCC
Power Factor	PF
Protective Extra Low Voltage	PELV
Rated Inverter Output Current	linv
Reactive Power	Q
Revolutions Per Minute	RPM
Second	S
Short circuit ratio	Rsce
Total Demand Distortion	TDD
Total Harmonic Distortion	THD
Total Harmonic Current Distortior	THiD
Total Harmonic Voltage Distortior	THvD
True Power Factor	TPF
Volts	V
IVLT,MAX	The maximum output current.
I _{VLT,N}	The rated output current
	supplied by the frequency
	converter.





Equipment containing electrical components may not be disposed of together with domestic waste. It must be separately collected with electrical and electronic waste according to local and currently valid legislation.



2.1.3 CE Conformity and Labelling

What is CE Conformity and Labelling?

The purpose of CE labelling is to avoid technical trade obstacles within EFTA and the EU. The EU has introduced the CE label as a simple way of showing whether a product complies with the relevant EU directives. The CE label says nothing about the specifications or quality of the product. The low-voltage directive (73/23/EEC)

Frequency converters must be CE labelled in accordance with the low-voltage directive of January 1, 1997. The directive applies to all electrical equipment and appliances used in the 50 - 1000 V AC and the 75 - 1500 V DC voltage ranges. Danfoss CE-labels in accordance with the directive and issues a declaration of conformity upon request.

2.1.4 Warnings



WARNING

Improper installation of the filter or the frequency converter may cause equipment failure, serious injury or death. Follow this Design Guide and install according to National and Local Electrical Codes.



WARNING

Never work on a filter in operation. Touching the electrical parts may be fatal - even after the equipment has been disconnected from the drive or motor.



WARNING

Before disconnecting the filter, wait at least the voltage discharge time stated in the Design Guide for the corresponding frequency converter to avoid electrical shock hazard.



CAUTION

When in use the filter surface temperature rises. DO NOT touch filter during operation.



CAUTION

To prevent resonances in the DC-link, it is recommended to disable the dynamic DC-link compensation by setting par. 14-51 to OFF.Se chapter *Ho to Programme the Frequency Converter*.



CAUTION

Temperature contactor must be used to prevent damage of the filter caused by over temperature. An immediate stop or a controlled ramp down within 30 seconds has to be performed to prevent filter damage.

NOTE

Never attempt to repair a defect filter.

NOTE

The filters represented in this Design Guide are specially designed and tested for operation with Danfoss frequency converters (FC 102/202/301 and 302) Danfoss takes no responsibility for the use of the filters with third party frequency converters.



WARNING

Non - authorized removal of required cover, inappropriate use, incorrect installation or operation, creates the risk of severe injury to persons or damage to material assets.



CAUTION

All operations concerning transport, installation and commissioning as well as maintenance must be carried out by qualified, skilled personnel (IEC 60364 and CENELEC HD 384 or IEC 60364 and IEC-Report 664 or DIN VDE 0110. National regulations for the prevention of accidents must be observed).

NOTE

According to this basic safety information qualified skilled personnel are persons who are familiar with the assembly, commissioning and operation of the product and who have the qualifications necessary for their occupation.



NOTE

The filters are components, that are designed for installation in electrical systems or machinery. When installing in machines, commissioning of the filters (i.e. the starting of operation as directed) is prohibited until it is proven, that the machine corresponds to the regulations of the EC Directive 83/392/EEC (Machinery Directive); EN 60204 must be observed.

NOTE

Commissioning (i.e. starting operation as directed) is only allowed when there is compliance with the EMC-Directive 89/336/EEC.

The filters meet the requirements of the Low-Voltage Directive 73/23/EEC. The technical data and information on the connection conditions must be obtained from the nameplate and the documentation and must be observed in all cases.

NOTE

The filter must be protected from inappropriate loads. In particular; during transport and handling: Components are not allowed to be bent. Distance between isolation must not be altered. Touching of electronic components and contacts must be avoided.

NOTE

When measuring on live filters, the valid national regulations for the prevention of accidents (e.g. VBG 4) must be observed.

The electrical installation must be carried out according to the appropriate regulations (e.g. cable cross-sections, fuses, PE-connection). When using the filters with frequency converters without safe separation from the supply line (to VDE 0100) all control wiring has to be included in further protective measures (e.g. double insulated or shielded, grounded and insulated).

NOTE

Systems where filters are installed, if applicable, have to be equipped with additional monitoring and protective devices according to the valid safety regulations e.g. law on technical tools, regulations for the prevention of accidents, etc.



3 Introduction to Harmonics and Mitigation

3.1 What are Harmonics?

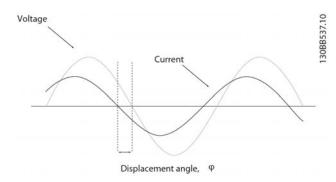
3.1.1 Linear Loads

On a sinusoidal AC supply a purely resistive loads (for example an incandescent light bulb) will draw a sinusoidal current, in phase with the supply voltage.

The power dissipated by the load is:

 $P = U \times I$

For reactive loads (such as an induction motor) the current will no longer be in phase with the voltage, but will lag the voltage creating a lagging true power factor with a value less than 1. In the case of capacitive loads the current is in advance of the voltage, creating a leading true power factor with a value less than 1.



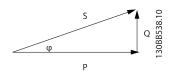
In this case, the AC power has three components: real power (P), reactive power (Q) and apparent power (S). The apparent power is:

 $S = U \times I$

(where S=[kVA], P=[kW] and Q=[kVAR])

In the case of a perfectly sinusoidal waveform P, Q and S can be expressed as vectors that form a triangle:

$$s^2 = P^2 + Q^2$$



The displacement angle between current and voltage is ϕ . The displacement power factor is the ratio between the active power (P) and apparent power (S):

$$DPF = \frac{P}{S} = cos(\varphi)$$

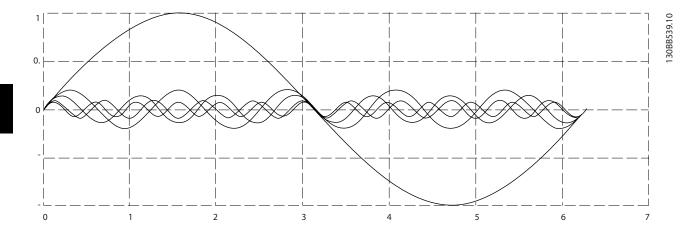
3.1.2 Non-linear Loads

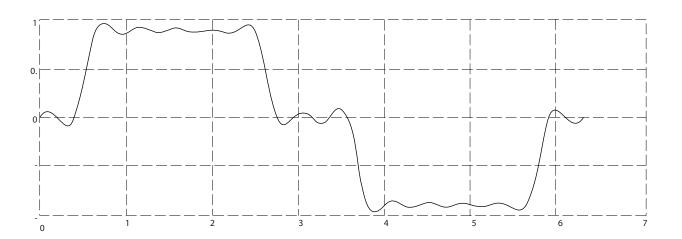
Non-linear loads (such as diode rectifiers) draw a non-sinusoidal current. The figure below shows the current drawn by a 6-pulse rectifier on a three phase supply.

A non-sinusoidal waveform can be decomposed in a sum of sinusoidal waveforms with periods equal to integer multiples of the fundamental waveform.

$$f(t) = \sum a_h \times sin(h\omega_1 t)$$

See following illustrations.





The integer multiples of the fundamental frequency $\omega 1$ are called harmonics. The RMS value of a non-sinusoidal waveform (current or voltage) is expressed as:

$$I_{RMS} = \sqrt{\frac{h_{max}}{\sum_{h=1}^{\infty} I_{(h)}^2}}$$

The amount of harmonics in a waveform gives the distortion factor, or total harmonic distortion (THD), represented by the ratio of RMS of the harmonic content to the RMS value of the fundamental quantity, expressed as a percentage of the fundamental:

$$THD = \sqrt{\frac{h_{max}}{\sum_{h=2}^{L} \left(\frac{I_h}{I_1}\right)^2}} \times 100\%$$

Using the THD, the relationship between the RMS current I_{RMS} and the fundamental current I_{1} can be expressed as:

$$I_{RMS} = I_1 \times \sqrt{1 + THD^2}$$

The same applies for voltage.

The true power factor PF (λ) is:

$$PF = \frac{P}{S}$$

In a linear system the true power factor is equal to the displacement power factor:

$$PF = DPF = cos(\varphi)$$

In non-linear systems the relationship between true power factor and displacement power factor is:

$$PF = \frac{DPF}{\sqrt{1 + THD^2}}$$

The power factor is decreased by reactive power and harmonic loads. Low power factor results in a high RMS current that produces higher losses in the supply cables and transformers.

In the power quality context, the total demand distortion (TDD) term is often encountered. The TDD does not characterize the load, but it is a system parameter. TDD expresses the current harmonic distortion in percentage of the <u>maximum</u> demand current lie.

$$TDD = \sqrt{\frac{h_{max}}{\sum_{h=2}^{L} \left(\frac{I_h}{I_I}\right)^2} \times 100\%}$$

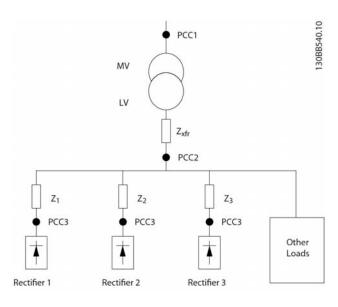
Another term often encountered in literature is the partial weighted harmonic distortion (PWHD). PWHD represents a weighted harmonic distortion that contains only the harmonics between the 14th and the 40th, as shown in the following definition:



$$PWHD = \sqrt{\frac{40}{\sum_{h=14}^{2}} \left(\frac{I_h}{I_1}\right)^2} \times 100\%$$

3.1.3 The Effect of Harmonics in a Power Distribution System

The figure below shows an example of a small distribution system. A transformer is connected on the primary side to a point of common coupling PCC1, on the medium voltage supply. The transformer has an impedance Z_{xfr} and feeds a number of loads. The point of common coupling where all loads are connected together is PCC2. Each load is connected through cables that have an impedance Z_1 , Z_2 , Z_3 .



Harmonic currents drawn by non-linear loads cause distortion of the voltage because of the voltage drop on the impedances of the distribution system. Higher impedances result in higher levels of voltage distortion.

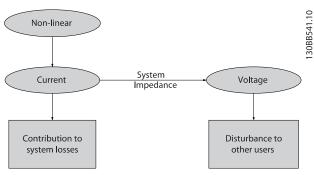
Current distortion relates to apparatus performance and it relates to the individual load. Voltage distortion relates to system performance. It is not possible to determine the voltage distortion in the PCC knowing only the load's harmonic performance. In order to predict the distortion in the PCC the configuration of the distribution system and relevant impedances must be known.

A commonly used term for describing the impedance of a grid is the short circuit ratio R_{sce} , defined as the ratio between the short circuit apparent power of the supply at the PCC (S_{sc}) and the rated apparent power of the load (S_{equ}):

$$R_{sce} = \frac{s_{ce}}{s_{equ}}$$
where $s_{sc} = \frac{u^2}{z_{supply}}$ and $s_{equ} = u \times t_{equ}$

The negative effect of harmonics is twofold:

- Harmonic currents contribute to system losses (in cabling, transformer)
- Harmonic voltage distortion causes disturbance to other loads and increase losses in other loads



3.2 Harmonic Limitation Standards and Requirements

The requirements for harmonic limitation can be:

- Application specific requirements
- Requirements from standards that have to be observed

The application specific requirements are related to a specific installation where there are technical reasons for limiting the harmonics.

For example on a 250 kVA transformer with two 110 kW motors connected. One is connected direct on-line and the other one is supplied through a frequency converter. If the direct on-line motor should also be supplied through a frequency converter the transformer will, in this case, be undersized. In order to retrofit, without changing the transformer, the harmonic distortion from the two drives has to be mitigated using AHF filters.

There are various harmonic mitigation standards, regulations and recommendations. Different standards apply in different geographical areas and industries. The following four commonly encountered standards will be presented:

- IEC61000-3-2
- IEC61000-3-12
- IEC61000-3-4
- IEEE 519
- G5/4



IEC61000-3-2, Limits for harmonic current emissions (equipment input current ≤ 16 A per phase)

The scope of IEC61000-3-2 is equipment connected to the public low-voltage distribution system having an input current up to and including 16 A per phase. Four emission classes are defined: Class A through D. The VLT drives are in Class A. However, there are no limits for professional equipment with a total rated power greater than 1 kW.

IEC61000-3-12, Limits for harmonic currents produced by equipment connected to public low-voltage systems with input current >16 A and ≤75 A

The scope of IEC61000-3-12 is equipment connected to the public low-voltage distribution system having an input current between 16 A and 75 A. The emission limits are currently only for 230/400 V 50 Hz systems and limits for other systems will be added in the future. The emission limits that apply for drives are given in Table 4 in the standard. There are requirements for individual harmonics (5th, 7th, 11th, and 13th) and for THD and PWHD. Frequency converters from the Automation Drive series (FC 102 HVAC, FC 202 Aqua and FC 302 Industry) comply with these limits without additional filtering.

IEC61000-3-4, Limits, Limitation of emission of harmonic currents in low-voltage power supply systems for equipment with rated current greater than 16 A

IEC61000-3-12 supersedes IEC61000-3-4 for currents up to 75 A. Therefore the scope of IEC61000-3-4 is equipment with rated current greater than 75 A connected to the public low-voltage distribution system. It has the status of *Technical report* and should not be seen as an international standard. A three-stage assessment procedure is described for the connection of equipment to the public supply and equipment above 75 A is limited to stage 3 *connection based on the load's agreed power*. The supply authority may accept the connection of the equipment on the basis of the agreed active power of the load's installation and local requirements of the power supply authority apply. The manufacturer shall provide individual harmonics and the values for THD and PWHD.

IEEE519, IEEE recommended practices and requirements for harmonic control in electrical power systems

IEEE519 establishes goals for the design of electrical systems that include both linear and nonlinear loads. Waveform distortion goals are established and the interface between sources and loads is described as point of common coupling (PCC).

IEEE519 is a system standard that aims the control of the voltage distortion at the PCC to a THD of 5 % and limits the maximum individual frequency voltage harmonic to 3 %. The development of harmonic current limits aims the limitation of harmonic injection from individual customers so they will not cause unacceptable voltage distortion levels and the limitation of the overall harmonic distortion of the system voltage supplied by the utility.

The current distortion limits are given in Table 10.3 in the standard and depend on the ratio I_{SC}/I_L where I_{SC} is the short circuit current at the utility PCC and I_L is the maximum demand load current. The limits are given for individual harmonics up to the 35th and total demand distortion (TDD).

Please note that these limits apply at the PCC to the utility. While requiring individual loads to comply with these limits also ensures the compliance at the PCC, this is rarely the most economic solution, being unnecessarily expensive. The most effective way to meet the harmonic distortion requirements is to mitigate at the individual loads and measure at the PCC.

However, if in a specific application it is required that the individual drive should comply with the IEEE519 current distortion limits, an AHF can be employed to meet these limits.

G5/4, Engineering recommendation, planning levels for harmonic voltage distortion and the connection of non-linear equipment to transmission systems and distribution networks in the United Kingdom

G5/4 sets planning levels for harmonic voltage distortion to be used in the process of connecting non-linear equipment. A process for establishing individual customer emission limits based on these planning levels is described. G5/4 is a system level standard.

For 400 V the voltage THD planning level is 5 % at the PCC. Limits for odd and even harmonics in 400 V systems are given in Table 2 in the standard. An assessment procedure for the connection of non-linear equipment is described. The procedure follows three stages, aiming to balance the level of detail required by the assessment process with the degree of risk that the connection of particular equipment will result in unacceptable voltage harmonic distortion.

Compliance of a system containing VLT[®] frequency converters depends on the specific topology and population of nonlinear loads. AHF can be employed to meet the requirements of G5/4.

3.3 Harmonic Mitigation

To mitigate the harmonics caused by the frequency converter 6-pulse recitifier several solutions exist and they all have their advantages and disadvantages. The choice of the right solution depends on several factors:

- The grid (background distortion, mains unbalance, resonance and type of supply - transformer/generator)
- Application (load profile, number of loads and load size)
- Local/national requirements/regulations (IEEE519, IEC, G5/4, etc.)
- Total cost of ownership (initial cost, efficiency, maintenance, etc.)

Harmonic solutions can be divided into two main categories: passive and active. Where the passive solutions consist of capacitors, inductors or a combination of the two in different arrangements.





The simplest solution is to add inductors/reactors of typically 3 % to 5 % in front of the frequency converter. This added inductance reduces the amount of harmonic currents produced by the drive. More advanced passive solutions combine capacitors and inductors in trap arrangement specially tuned to eliminate harmonics starting from e.g. the 5th harmonic.

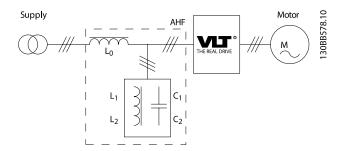
The active solutions determine the exact current that would cancel the harmonics present in the circuit and synthesizes and injects that current into the system. Thus the active solution can mitigate the real-time harmonic disturbances, which makes these solutions very effective at any load profile. To read more about the Danfoss active solutions Low Harmonic Drive (LHD) or Active Filters (AAF) please see MG.34.Ox.yy and MG.90.Vx.yy.

4

4 Introduction to Advanced Harmonic Filters

4.1 Operation Principle

The Danfoss Advanced Harmonic Filters (AHF) consist of a main inductor L_0 and a two-stage absorption circuit with the inductors L_1 and L_2 and the capacitors C_1 and C_2 . The absorption circuit is specially tuned to eliminate harmonics starting with the 5^{th} harmonic and is specific for the designed supply frequency. Consequently the circuit for 50 Hz has different parameters than the circuit for 60 Hz.



AHFs are available in two variants for two performance levels: AHF005 with 5 % THiD (total current harmonic distortion) and AHF010 with 10 % THiD. The strategy behind the two levels is to offer a performance similar to 12 pulse rectifiers with the AHF010 and a performance similar to 18 pulse rectifiers with AHF005.

The filter performance in terms of THiD varies as a function of the load. At nominal load the performance of the filter should be equal or better than 10 % THiD for AHF010 and 5 % THiD for AHF005.

At partial load the THiD has higher values. However, the absolute value of the harmonic current is lower at partial loads, even if the THiD has a higher value. Consequently, the negative effect of the harmonics at partial loads will be lower than at full load.

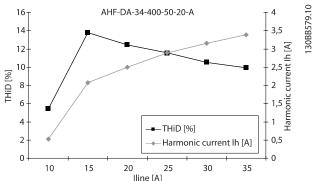
Example:

An 18.5 kW drive is installed on a 400 V/50 Hz grid with a 34 A AHF010 (type code AHF-DA-34-400-50-20-A).

Following values are measured for different load currents, using a harmonic analyzer:

I line RMS [A]	Fundamental current at 50 Hz I ¹ RMS [A]	THID [%]	Total harmonic current lh RMS [A] ¹
9.6	9.59	5.45	0.52
15.24	15.09	13.78	2.07
20.24	20.08	12.46	2.5
25.17	25	11.56	2.89
30.27	30.1	10.5	3.15
34.2	34.03	9.95	3.39

¹)The total harmonic current has been calculated. The THiD vs. load plot is shown in the following figure:



It can be observed that at partial load, 15 A, the THiD is approximately 14 %, compared to 10 % at the nominal load of 34 A. On the other hand, the total harmonic current is only 2.07 A at 15 A line current against 3.39 A harmonic current at 34 A line current. Thus, THiD is only a relative indicator of the harmonic performance. The harmonic distortion of the voltage will be less at partial load than at nominal load.

Factors such as background distortion and grid unbalance can affect the performance of AHF filters. The specific figures are different from filter to filter and the graphs below show typical performance characteristics. For specific details a harmonic design tool such as MCT 31 or Harmonic Calculation Software (HCS) should be used.

Background distortion: The design of the filters aims to achieve 10 % respectively 5 % THiD levels with a background distortion of THvD = 2 %. Practical measurements on typical grid conditions in installations with frequency converters show that often the performance of the filter is slightly better with a 2 % background distortion. However, the complexity of the grid conditions and mix of specific harmonics can not allow a general rule about the performance on a distorted grid. Therefore we have chosen to present worst-case performance deterioration characteristics with the background distortion.



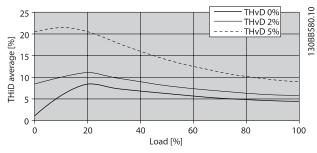


Illustration 4.1: AHF005

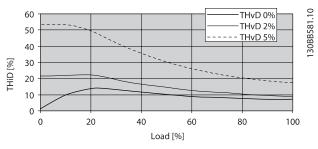


Illustration 4.2: AHF010

Performance at 10% THvD has not been plotted. However, the filters have been tested and can operate at 10% THvD but the filter performance can no longer be guaranteed.

The filter performance also deteriorates with the unbalance of the supply. Typical performance is shown in the graphs below:

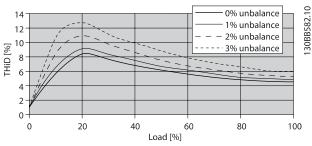


Illustration 4.3: AHF005

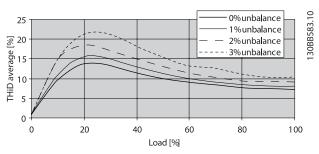


Illustration 4.4: AHF010

4.1.1 Power Factor

In no load conditions (the frequency converter is in stand-by) the frequency converter current is negligible and the main current drawn from the grid is the current through the capacitors in the harmonic filter. Therefore the power factor is close to 0, capacitive. The capacitive current is approximately 25 % of the filter nominal current (depends on filter size, typical values between 20 and 25 %). The power factor increases with the load. Because of the higher value of the main inductor L0 in the AHF005, the power factor is slightly higher than in the AHF010.

Following graphs show typical values for the true power factor on AHF010 and AHF005.

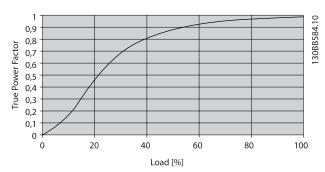


Illustration 4.5: AHF005

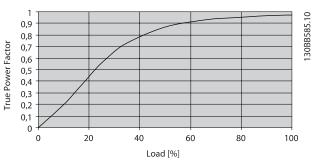


Illustration 4.6: AHF010

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4.1.2 Capacitor Disconnect

If the specific application requires a higher power factor at noload and the reduction of the capacitive current in stand-by, a capacitor disconnect should be used. A contactor disconnects the capacitor at loads below 20 %. It is important to note that the capacitors may not be connected at full load or disconnected at no load.

It is very important to consider the capacitive current in the design of applications where the harmonic filter is supplied by a generator. The capacitive current can overexcite the generator in no-load and low-load condition. The over-excitation causes an increase of the voltage that can exceed the allowed voltage for the AHF and the frequency converter. Therefore a capacitor disconnect should always be used in generator applications and the design carefully considered.

Compared to multi-pulse rectifiers, passive harmonic filter (such as AHF) are more robust against background distortion and supply imbalance. However, the performance of passive filters is inferior to the performance of active filters when it comes to partial load performance and power factor. For details about the performance positioning of the various harmonic mitigation solutions offered by Danfoss, please consult the relevant harmonic mitigation literature.



5 Selection of Advanced Harmonic Filter

This chapter will provide guidance about how to choose the right filter size and contains calculation examples, electrical data and the general specification of the filters.

5.1 How to Select the Correct AHF

For optimal performance the AHF should be sized for the mains input current to the frequency converter. This is the input current drawn based on the expected load of the frequency converter and not the size of the frequency converter itself.

5.1.1 Calculation of the Correct Filter Size Needed

The mains input current of the frequency converter ($I_{FC,L}$) can be calculated using the nominal motor current ($I_{M,N}$) and the displacement factor (Cos ϕ) of the motor. Both values are normally printed on the name plate of the motor. In case the nominal motor voltage ($U_{M,N}$) is unequal to the actual mains voltage (U_L), the calculated current must be corrected with the ratio between these voltages as shown in the following

equation:
$$I_{FC.L} = 1.1 \times I_{M,N} \times cos(\rho) \times \frac{U_{M,N}}{U_L}$$

The AHF chosen must have a nominal current ($I_{AHF,N}$) equal to or larger than the calculated frequency converter mains input current (I_{FCL}).

NOTE

Do not oversize the AHF. The best harmonic performance is obtained at nominal filter load. Using an oversized filter will most likely result in reduced THiD performance.

If several frequency converters are to be connected to the same filter, the AHF must be sized according to the sum of the calculated mains input currents.

NOTE

If the AHF is sized for a specific load and the motor is changed, the current must be recalculated to avoid overloading the AHF.

5.1.2 Calculation Example

System mains voltage (U _L):	380 V
Motor name plate power(P _M):	55 kW
Motor efficiency (η_M):	0.96
FC efficiency (η _{FC}):	0.97
AHF effiency (η _{AHF})(worst case estimate):	0.98

Maximum line current (RMS):

$$\frac{P_M \times 1000}{U_L \times \eta_M \times \eta_{FC} \times \eta_{AHF} \times \sqrt{3}} = \frac{55 \times 1000}{380 \times 0.96 \times 0.97 \times 0.98 \times \sqrt{3}} = 91.57 \text{ A}$$
In this case a 96 A filter must be chosen.



5.2 Electrical Data

380 V - 415 V, 50 Hz

	-				-	•		•		
Code number AHF005	Code number AHF010	riiter current rating	ı ypıcaı motor	VLI power and current ratings	ina current	Losses AHF005	AHE010	Acoustic noise	rrame size	บ
IP00/IP20	IP00/IP20	S V	kW	kW	¥	*	*	dBA	AHF005	AHF010
130B1392	130B1262	10	æ	PK37-P4K0	1.2-9	131	93	<70	×	×
130B1229	130B1027									
130B1393	130B1263	14	7.5	P5K5-P7K5	14.4	184	118	<70	× - -	×
13081231	13081058	C	7	7,	C	C	700	Ç	S	Ş
130B1232	130B1059	77	Ξ	주 두	77	857	907	0/>	X	X
130B1395	130B1270	29	15	P15K	29	298	224	<70	X2	X2
130B1233	130B1089									
130B1396	130B1273	34	18.5	P18K	34	335	233	<72	X3	X3
130B1238	130B1094									
130B1397	130B1274	40	22	P22K	40	396	242	<72	X3	X3
130B1239	130B1111									
130B1398	130B1275	55	30	P30K	55	482	274	<72	X3	X3
130B1240	130B1176									
130B1399	130B1281	99	37	P37K	99	574	352	<72	X4	X4 X4
130B1241	130B1180									
130B1442	130B1291	82	45	P45K	82	889	374	<72	X4	X4
130B1247	130B1201									
130B1443	130B1292	96	55	P55K	96	747	428	<75	X5	X5
130B1248	130B1204									
130B1444	130B1293	133	75	P75K	133	841	488	<75	X5	X5
130B1249	130B1207									
130B1445	130B1294	171	06	P90K	171	962	692	<75	9X	9X
130B1250	130B1213									
130B1446	130B1295	204	110	P110	204	1080	742	<75	9X	9X
130B1251	130B1214									
130B1447	130B1369	251	132	P132	251	1195	864	<75	X7	X7
130B1258	130B1215									
130B1448	130B1370	304	160	P160	304	1288	905	<75	X7	×
130B1259	130B1216									
130B1449	130B1389	381	200	P200	381	1510	1175	<77	X8	X7
130B1260	130B1217									
130B1469	130B1391	480	250	P250	472	1852	1542	<77>	8X	X8
130B1261	130B1228									

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Code number AHF005	Code number AHF010	Filter current rating	Typical motor VLT power and current ratings	VLT power and current ratings	and	Losses AHF005	AHF010	Acoustic noise	Frame size
IP00/IP20	IP00/IP20	· ⋖	kW	ΚW	· «		*	dBA	AHF00 AHF010 5
2 x 130B1448 2 x 130B1259	2 x 130B1370 2 x 130B1216	809	315	P315	290	2576	1810	<80	
2 x 130B3153 2 x 130B3152	2 x 130B3151 2 x 130B3136	650	355	P355	647	2812	1904	<80	
130B1448 + 130B1449 130B1259 + 130B1260	130B1370 + 130B1389 130B1216 + 130B1217	685	400	P400	684	2798	2080	<80	
2 x 130B1449 2 x 130B1260	2 x 130B1389 2 x 130B1217	762	450	P450	779	3020	2350	<80	
130B1449 + 130B1469 130B1260 + 130B1261	130B1389 + 130B1391 130B1217 + 130B1228	861	500	P500	857	3362	2717	<80	
2 x 130B1469 2 x 130B1261	2 x 130B1391 2 x 130B1228	096	560	P560	964	3704	3084	<80	
3 x 130B1449 3 x 130B1260	3 x 130B1389 3 x 130B1217	1140	630	P630	1090	4530	3525	<80	
2 x 130B1449 + 130B1469 2 x 130B1260 + 130B1261	2 x 130B1389 + 130B1391 2 x 130B1217 + 130B1228	1240	710	P710	1227	4872	3892	<80	
3 x 130B1469 3 x 1301261	3 x 130B1391 3 x 130B1228	1440	800	P800	1422	5556	4626	<80	
2 x 130B1449 + 2 x 130B1465 2 x 130B1260 + 2 x 130B1261	2 x 130B1449 + 2 x 130B1469 2 x 130B1389 + 2 x 130B1391 1720 2 x 130B1260 + 2 x 130B1261 2 x 130B1217 + 2 x 130B1228	1720	1000	P1000	1675	6724	5434	<80	

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380 V - 415 V, 60 Hz

Cade annah an	C. d A. 15040	Tilker and	T. milant makes	F 57	4 m m m			() () () () () () () () () ()	100	
AHE005	IP00/IP20	riiter current	iypicai motor	vLi power and current ratings	ınd current	Losses AHF005	AHE010	Acoustic noise	riaine size	υ
IP00/IP20		6 •	kW	KW	⋖	*	*	dBA	AHF005	AHF010
130B3095	130B2874	10	3	PK37-P4K0	1.2-9	131	93	<70	×	X
130B1257	130B2262									
130B3096	130B2875	14	7.5	P5K5-P7K5	14.14	184	118	<70	X	X X
130B2858	130B2265									
130B3097	130B2876	22	11	P11K	22	258	206	<70	X2	X2
130B2859	130B2268									
130B3098	130B2877	29	15	P15K	29	298	224	<70	X2	X
130B2860	130B2294									
130B3099	130B3000	34	18.5	P18K	34	335	233	<72	X3	X3
130B2861	130B2297									
130B3124	130B3083	40	22	P22K	40	396	242	<72	X3	X3
130B2862	130B2303									
130B3125	130B3084	55	30	P30K	55	482	274	<72	X3	X3
130B2863	13082445									
130B3026	130B3085	99	37	P37K	99	574	352	<72	X4	X4
130B2864	130B2459									
130B3127	130B3086	82	45	P45K	82	688	374	<72	**	X4
130B2865	130B2488									
130B3128	130B3087	96	55	P55K	96	747	427	<75	X5	X5
130B2866	130B2489									
130B3129	130B3088	133	75	P75K	133	841	488	<75	X5	X5
130B2867	130B2498									
130B3130	130B3089	171	06	P90K	171	962	692	<75	9X	9X
130B2868	130B2499									
130B3131	130B3090	204	110	P110	204	1080	743	<75	9X	9X
130B2869	130B2500									
130B3132	130B3091	251	132	P132	251	1194	864	<75	X7	X
130B2870	130B2700									
130B3133	130B3092	304	160	P160	304	1288	902	<75	×	X
13082871	130B2819									
130B3134	130B3093	381	200	P200	381	1510	1175	<77	X8	X8
13082872	130B2855									
130B3135	130B3094	480	250	P250	472	1850	1542	<77	X8	X8
130B2873	130B2856									



Code number AHF005	Codenumber AHF010	Filter current	Typical	VLT power	VLT power and current Losses	Losses		Acoustic noise	Frame size
IP00/IP20	IP00/IP20	rating	motor	ratings		AHF005	AHF010		
		⋖	kW	kW	⋖	>	>	dBA	AHF005 AHF010
2 x 130B3133	2 x 130B3092	809	315	P315	290	2576	1810	<80	
2 x 130B2871	2 x 130B2819								
2 x 130B3157	2 x 130B3155	029	315	P355	647	2812	1904	<80	
2 x 130B3156	2 x 130B3154								
130B3133 + 130B3134	130B3092 + 130B3093	685	355	P400	684	2798	2080	<80	
130B2871 + 130B2872	130B2819 + 130B2855								
2 x 130B3134	2 x 130B3093	762	400	P450	779	3020	2350	<80	
2 x 130B2872	2 x 130B2855								
130B3134 + 130B3135	130B3093 + 130B3094	861	450	P500	857	3362	2717	<80	
130B2872 + 130B3135	130B2855 + 130B2856								
2 x 130B3135	2 x 130B3094	096	500	P560	964	3704	3084	<80	
2 x 130B2873	2 x 130B2856								
3 x 130B3134	3 x 130B3093	1140	260	P630	1090	4530	3525	<80	
3 x 130B2872	3 x 130B2855								
2 x 130B3134 + 130B3135	2 x 130B3093 + 130B3094	1240	630	P710	1227	4872	3892	<80	
2 x 130B2872 + 130B2873	2 x 130B2855 + 130B2856								
3 x 130B3135	3 x 130B3094	1440	710	P800	1422	5556	4626	<80	
3 x 130B2873	3 x 130B2856								
2 x 130B3134 + 2 x 130B3135	2 x 130B3134 + 2 x 130B3135 2 x 130B3093 + 2 x 130B3094 1722		800	P1000	1675	6724	5434	<80	
2 x 130B2872 + 2 x 130B2873	2 x 130B2872 + 2 x 130B2873 2 x 130B2855 + 2 x 130B2856								

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440 V - 480 V, 60 Hz

and and a		Tilker of the		T 1/1	4			A colour citorion	1000	
AHF005	AHF010	riiter Curreiit rating	iypical motor	vei power and current ratings	ומ כמוופוור	AHF005	AHF010	Acoustic Hoise	רומוווה אבה	1)
IP00/IP20	IP00/IP20	· •	kw	ΚW	V	>	*	dBA	AHF005	AHF010
130B1787	130B1770	10	я	PK37-P4K0	1-7.4	131	93	<70	×	×
130B1752	130B1482									
130B1788	130B1771	17	7.5	P5K5-P7K5	9.9+13	184	188	<70	×	×
130B1753	130B1483									
130B1789	130B1772	19	11	P11K	19	258	206	<70	X2	X2
130B1754	130B1484									
130B1790	130B1773	25	15	P15K	25	298	224	<70	X2	X2
130B1755	130B1485									
130B1791	130B1774	31	18.5	P18K	31	335	233	<72	X3	X3
130B1756	130B1486									
130B1792	130B1775	36	22	P22K	36	396	242	<72	X3	X3
130B1757	130B1487									
130B1793	130B1776	48	30	P30K	47	482	374	<72	X3	X3
130B1758	130B1488									
130B1794	130B1777	09	37	P37K	59	574	352	<72	X4	X4
130B1759	130B1491									
130B1795	130B1778	73	45	P45K	73	889	374	<72	**	X 4x
130B1760	130B1492									
130B1796	130B1779	95	55	P55K	95	747	428	<75	X5	X5
130B1761	130B1793									
130B1797	130B1780	118	75	P75K	118	841	488	<75	X5	X5
130B1762	130B1494									
130B1798	130B1781	154	06	P90K	154	362	692	<75	9X	9X
130B1763	130B1495									
130B1799	130B1782	183	110	P110	183	1080	743	<75	9X	9X
130B1764	130B1496									
130B1900	130B1783	231	132	P132	231	1194	864	<75	X7	X7
130B1765	130B1497									
130B2200	130B1784	291	160	P160	291	1288	905	<75	X	X
130B1766	130B1498									
130B2257	130B1785	355	200	P200	348	1406	952	<75	X8	X8
130B1768	130B1499									
130B2259	130B1786	436	250	P250	436	1852	1542	<77>	X8	×
130B1769	130B1751									



Code number AHF005	Code number AHF010	Filter current	Typical	VLT power	VLT power and current Losses	Losses		Acoustic noise	Frame size
IP00/IP20	IP00/IP20		motor	ratings		AHF005	AHF010		
		4	kw	ΚW	⋖	>	>	dBA	AHF005 AHF010
130B1900 + 130B2200	130B1783 + 130B1784	522	315	P315	531	2482	1769	<80	
130B1765 + 130B1766	130B1497 + 130B1498								
2 x 130B2200	2 x 130B1784	582	355	P355	580	2576	1810	<80	
2 x 130B1766	2 x 130B1498								
130B2200 + 130B3166	130B1784 + 130B3166	671	400	P400	299	2798	2080	<80	
130B1766 + 130B3167	130B1498 + 130B3165								
2 x 130B2257	2 x 130B1785	710	450	P450	711	2812	1904	<80	
2 x 130B1768	2 x 130B1499								
2 x 130B3168	2 x 130B3166	760	200	P500	759	3020	2350	<80	
2 x 130B3167	2 x 130B3165								
2 x 130B2259	2 x 130B1786	872	260	P560	867	3704	3084	<80	
2 x 130B1769	2 x 130B1751								
3 x 130B2257	3 x 130B1785	1065	630	P630	1022	4218	2856	<80	
3 x 130B1768	3 x 130B1499								
3 x 130B3168	3 x 130B3166	1140	710	P710	1129	4530	3525	<80	
3 x 130B3167	3 x 130B3165								
3 x 130B2259	3 x 130B1786	1308	800	P800	1344	5556	4626	<80	
3 x 130B1769	3 x 130B1751								
2 x 130B2257 + 2 x 130B2259	2 x 130B2257 + 2 x 130B2259 2 x 130B1785 + 2 x 130B1786 1582	1582	1000	P1000	1490	6516	2988	<80	
2 x 130B1768 + 2 x 130B1768	$2 \times 130B1768 + 2 \times 130B1768 \ 2 \times 130B1499 + 2 \times 130B1751$								

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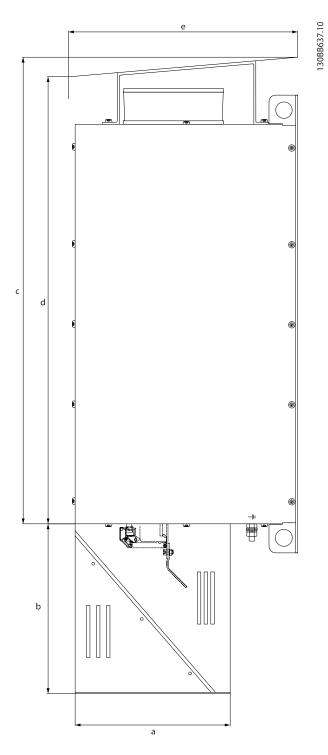
5.2.1 Accessories

IP21/NEMA1 enclosure kits for the IP20 filters are available and listed here:

Danfoss part number	IP21/NEMA1 kit for IP20 enclosure
130B3274	X1
130B3275	X2
130B3276	Х3
130B3277	X4
130B3278	X5
130B3279	X6
130B3281	X7
130B3282	X8

The kit consists of two parts:

A top plate that prevents vertically falling drops of water and dirt from entering the filter and a terminal cover ensuring touch safe terminals. The terminal cover is prepared for installation of a contactor for capacitor disconnect.



Enclosure type	а	b	с	d	e
	(mm)	(mm)	(mm)	(mm)	(mm)
X1	120	160	329.5	344.5	215.5
X2	190	180	433.5	448.5	257.5
Х3	145	210	543.5	558.5	252
X4	230	230	573.5	558.5	343
X5	230	250	681.5	696.5	343
X6	300	270	681.5	696.5	410
X7	300	320	796.5	811.5	458.5
X8	400	350	796.5	811.5	553



NOTE

The NEMA 1 cover is designed for the mounting of Danfoss contactors.

When using non Danfoss contactors, please observe the dimensions of the NEMA 1 terminal cover and ensure that there is space for the contactor.

5.3 General Specification

5.3.1 General Technical Data

Supply voltage tolerance	+/- 10 %
Supply frequency tolerance	+5 %/-1.5 %
Overload capability	160 % for 60 seconds
Efficiency	>0.98
THiD*	AHF005 < 5 %
	AHF010 < 10 %
Cos φ of I _L	0.5 cap at 25 % lahf,n
	0.8 cap at 50 % I _{AHF,N}
	0.85 cap at 75 % I _{AHF,N}
	0.99 cap at 100 % laнғ,n
	1.00 cap at 160 % I _{AHF,N}
Power derating	Temperature - see derating
	curve below.
	1000 m altitude above sea level
	< h < 2000 m = 5 % per 1000
	m

NOTE

The reduction of the low harmonic current emission to the rated THiD implies that the THvD of the non-influenced mains voltage is lower than 2% and the ratio of short circuit power to installed load (R_{SCE}) is at least 66. Under these conditions the THiD of the mains current of the frequency converter is reduced to 10 % or 5 % (typical values at nominal load). If these conditions are not or only partially fulfilled, a significant reduction of the harmonic components can still be achieved, but the rated THiD values may not be observed.

	Dimensions in mm				
Enclosure Type	A (height)	B (width)	C (depth)		
X1	332	190	206		
X2	436	232	248		
Х3	594	378	242		
X4	634	378	333		
X5	747	418	333		
X6	778	418	396		
X7	909	468	449		
X8	911	468	549		

Table 5.1: Enclosure dimensions

5.3.2 Environmental Data

Surroundings	
Ambient tempera-	5°C + 45°C - without derating
ture during full-scale	5°C + 60°C - with derating
operation	
Temperature during	-25°C + 65°C - transport
storage/transport	-25°C + 55°C - storage
Max. altitude above	1000 m (without derating)
sea level	Between 1000 m and 2000 m (with derating)
Max. relative	Humidity class F without condensation - 5 $\%$ -
humidity	85 % - Class 3K3 (non-sondensing) during
	operation
Insulation strength	Overvoltage category III according to
	ENG61800-5-1
Packaging	DIN55468 for transport packaging materials

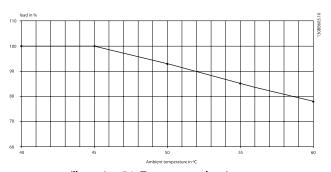


Illustration 5.1: Temperature derating curve



6 How to Install

6.1 Mechanical Mounting

6.1.1 Safety Requirements of Mechanical Installation

NOTE

Please observe the filter weight and ensure that proper lifting equipment is used.

NOTE

When installing the filter use the lifting eyes on both sides to lift the filter.

NOTE

Do not use other parts (terminals, enclosures, etc.).

6.1.2 Mounting

The filters are available in IP00 and IP20 and for both IP ratings the following guidance must be followed during installation:

- All filters must be mounted vertically with the terminals at the bottom
- Do not mount the filter close to other heating elements or heat sensitive material (such as wood)

IP00:

• The surface temperature of the IP00 filters can exceed 70°C and a hot surface warning label is placed on the filter

IP20:

- Top and bottom clearance is minimum 150 mm
- The surface temperature of the IP20 filters does not exceed 70°C
- The filter can be side-by-side mounted with the frequency converter and there is no requirement for spacing between then

6.1.3 Recommendations for Installation in Industrial Enclosures

To avoid high frequency noise coupling keep a minimum distance of 150 mm (5.91 inches) to:

- mains/supply wires
- motor wires of frequency converter
- control- and signal wires (voltage range < 48 V)

To obtain low impedance HF-connections, grounding, screening and other metallic connections (e.g. mounting plates, mounted units) should have a surface as large as possible to metallic ground. Use grounding and potential equalisation wires with a cross section as large as possible (min. 10 mm²) or thick grounding tapes. Use copper or tinned copper screened wires only, as steel screened wires are not suitable for high frequency applications. Connect the screen with metal clamps or metal glands to the equalisation bars or PE-connections.

Inductive switching units (relay, magnetic contactor etc.) must always be equipped with varistors, RC-circuits or suppressor diodes.

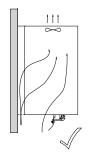
6.1.4 Ventilation

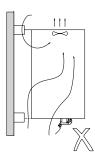
The filters are cooled by means of air circulation. Consequently the air needs to be able to move freely above and below the filter.

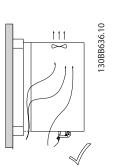
When mounting the filters in panels or other industrial enclosures it must be ensured that there is a sufficient airflow through the filter to reduce the risk of overheating the filter and the surrounding components.

If other heat sources (such as frequency converters) are installed in the same enclosure, the heat they generate also needs to be taken into account when dimensioning the cooling of the enclosure

The filters have to be mounted on a wall in order to guide air through the gap between the wall and the filter. In installations (e.g. panels) where the filter is mounted on rails, the filter will not be sufficiently cooled because of false airflow and therefore a back plate can be ordered separately. See following illustration.







Danfoss part number	Back plate
130B3283	X1
130B3284	X2
130B3285	Х3
130B3286	X4
130B3287	X5 and X6
130B3288	X7 and X8



6.2 Electrical Installation

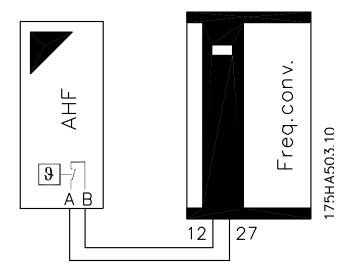
6.2.1 Over Temperature Protection

The Danfoss harmonic filters AHF005 and AHF010 are all equipped with a galvanic isolated switch (PELV) that is closed under normal operating conditions and open if the filter is overheated.

NOTE

The over temperature protection must be used to prevent damage of the filter caused by over temperature. An immediate stop or a controlled ramp down within max. 30 s has to be performed to prevent filter damage.

There are many ways the switch can be used and one example is to connect terminal A of the harmonic filter to terminal 12 or 13 (voltage supply digital input, 24 V) of the Danfoss frequency converter and terminal B to terminal 27. Program digital input terminal 27 to *Coast Inverse*. The frequency converter will coast the motor and thereby unload the filter if an over temperature is detected. Alternatively use terminal 12/33 and set par. 1-90 to *motor terminal protection*.



NOTE

The maximum rating of the over temperature contactor is 250 V AC and 10 A.

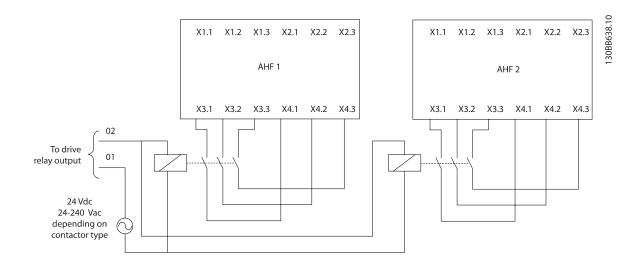
6.2.2 Capacitor Disconnect

The power factor of the harmonic filter AHF 005/010 is decreasing with decreasing load. At no load the power factor is zero and the capacitors produce leading current of approximately 25 % of rated the filter current. In applications where this reactive current is not acceptable the terminals X3.1, X3.2, X3.3 and X4.1, X4, X4.3 provide access to the capacitor bank, so it can be disconnected.

Default (on delivery) the wiring will shorten terminal X3.1 with X4.1, X3.2 with X4.2 and X3.3 with X.4.3. In the case that no capacitor disconnect is required, no changes should be made to these shorted terminals.

If a disconnection of the capacitors is required a three-phase contactor should be placed between terminals X3 and X4. It is recommended to use AC3 contactors.





NOTE

It is not allowed to use one common 3 poled contactor with several paralleled Advanced Harmonic Filters.

NOTE

The AHF filters in stand-by and under low load conditions, when the capacitors are not disconnected, boost the input voltage with up to 5 %. That means that the voltage at the drive terminals is up to 5 % higher than the voltage at the input of the filter. This should be considered at the design of the installation. Special care should be taken in 690 V applications where the voltage tolerance of the drive is reduced to + 5 %, unless a capacitor disconnect is used.

NOTE

Only switch the contactor at less than 20 % output power. Allow minimum 25 s for the capacitors to discharge before re-connecting

	Current		
Current rating	rating	Danfoss Contac-	
380-415 V, 50 and	440-480 V,	tors for AHF005	Alternative
60 Hz	60 Hz	and AHF010	type AC3
			Contactor
Α	Α	Type	rating ¹⁾ KVAr
10	10	CI 9	1
14	14	CI 9	2
22	19	CI 9	4
29	25	CI 9	6
34	31	CI 16	7
40	36	CI 16	7
55	48	CI 16	9
66	60	CI 61	11
82	73	CI 61	15
96	95	CI 61	17
133	118	CI 61	22
171	154	CI 61	29
204	183	CI 61	36
251	231	CI 110	44
304	291	CI 110	51
325	355	CI 110	58
380	380	CI 110	66
480	436	CI 141	88

¹⁾ min. 50 % of the nominal load



6.2.3 Wiring

Supply voltage must be connected to the terminals X1.1, X1.2 and X1.3. The frequency converter supply terminals L1, L2 and L3 must be connected to the filter terminals X2.1, X2.2 and X2.3

Paralleling of frequency converters

If several frequency converters are to be connected to one harmonic filter, the connection method is similar to the connection described above. The supply terminals L1, L2 and L3 of the frequency converters must be connected to the filter terminals X2.1, X2.2 and X2.3.

NOTE

Use cables complying with local regulations.

Paralleling of filters

If the mains input current of the frequency converter exceeds the nominal current of the largest harmonic filter, several harmonic filters can be paralleled to achieve the necessary current rating – see *Electrical Data* tabels.

Supply voltage be connected to the terminals X1.1, X1.2 and X1.3 of the filters. The frequency converter supply terminals L1, L2 and L3 must be connected to the filters terminals X2.1, X2.2 and X2.3

Terminals and cables

The following tabels show the terminal types, cable cross section, tightening torque, etc.

Main terminals				Capacitor disconnect terminals				
Current in A	Clamp	Cable cross-	Cable end	Torque in	Clamp capaci-	Cable cross-	Cable end	Torque in
	mains	section		Nm	tor disconnect	section		Nm
	terminals				terminals			
10	WDU 6	0.5-10 mm ²	cable end sleeve	1.6	WDU 2.5	0.5-4 mm ²	cable end sleeve	0.8
14	WDU 6	0.5-10 mm ²	cable end sleeve	1.6	WDU 2.5	0.5-4 mm ²	cable end sleeve	0.8
22	WDU 6	0.5-10 mm ²	cable end sleeve	1.6	WDU 2.5	0.5-4 mm ²	cable end sleeve	0.8
29	WDU 6	0.5-10 mm ²	cable end sleeve	1.6	WDU 2.5	0.5-4 mm ²	cable end sleeve	0.8
34	WDU 16	1.5-25 mm ²	cable end sleeve	2.4	WDU 10	1.5-16 mm ²	cable end sleeve	2.4
40	WDU 16	1.5-25 mm ²	cable end sleeve	2.4	WDU 10	1.5-16 mm ²	cable end sleeve	2.4
55	WDU 16	1.5-25 mm ²	cable end sleeve	2.4	WDU 10	1.5-16 mm ²	cable end sleeve	2.4
66	WDU 35	2.5-50 mm ²	cable end sleeve	4.5	WDU 16	1.5-16 mm ²	cable end sleeve	2.4
82	WDU 35	2.5-50 mm ²	cable end sleeve	4.5	WDU 16	1.5-16 mm ²	cable end sleeve	2.4
96	WDU 50 N	10-70 mm ²	cable end sleeve	6	WDU 16	1.5-16 mm ²	cable end sleeve	2.4
133	WDU 50 N	10-70 mm ²	cable end sleeve	6	WDU 16	1.5-16 mm ²	cable end sleeve	2.4
171	WFF 70	2.5-95 mm ²	cable lug M8	12	WDU 35	2.5-50 mm ²	cable end sleeve	4.5
204	WFF 70	2.5-95 mm ²	cable lug M8	12	WDU 35	2.5-50 mm ²	cable end sleeve	4.5
251	WFF 300	25-300 mm ²	cable lug M16	60	WDU 95 N	16-150 mm ²	cable end sleeve	20
304	WFF 300	25-300 mm ²	cable lug M16	60	WDU 95 N	16-150 mm ²	cable end sleeve	20
325	WFF 300	25-300 mm ²	cable lug M16	60	WDU 95 N	16-150 mm ²	cable end sleeve	20
380	WFF 300	25-300 mm ²	cable lug M16	60	WDU 95 N	16-150 mm ²	cable end sleeve	20
480	WFF 300	25-300 mm ²	cable lug M16	60	WDU 95 N	16-150 mm ²	cable end sleeve	20

Table 6.1: 380 - 415 V, 50 and 60 Hz



	Main terminals			Capacitor disconnect terminals				
Current in A	Clamp	Cable cross-	Cable end	Torque in	Clamp capaci-	Cable cross-	Cable end	Torque in Nm
	mains	section		Nm	tor disconnect	section		
	terminals				terminals			
10	WDU 6	0.5-10 mm ²	cable end sleeve	1.6	WDU 2.5	0.5-4 mm ²	cable end sleeve	0.8
14	WDU 6	0.5-10 mm ²	cable end sleeve	1.6	WDU 2.5	0.5-4 mm ²	cable end sleeve	0.8
19	WDU 6	0.5-10 mm ²	cable end sleeve	1.6	WDU 2.5	0.5-4 mm ²	cable end sleeve	0.8
25	WDU 6	0.5-10 mm ²	cable end sleeve	1.6	WDU 2.5	0.5-4 mm ²	cable end sleeve	0.8
31	WDU 16	1.5-25mm ²	cable end sleeve	2.4	WDU 10	1.5-16 mm ²	cable end sleeve	2.4
36	WDU 16	1.5-25mm ²	cable end sleeve	2.4	WDU 10	1.5-16 mm ²	cable end sleeve	2.4
48	WDU 16	1.5-25mm ²	cable end sleeve	2.4	WDU 10	1.5-16 mm ²	cable end sleeve	2.4
60	WDU 35	2.5-50 mm ²	cable end sleeve	4.5	WDU 16	1.5-25 mm ²	cable end sleeve	2.4
73	WDU 35	2.5-50 mm ²	cable end sleeve	4.5	WDU 16	1.5-25 mm ²	cable end sleeve	2.4
95	WDU 50 N	10-70 mm ²	cable end sleeve	6	WDU 16	1.5-25 mm ²	cable end sleeve	2.4
118	WDU 50 N	10-70 mm ²	cable end sleeve	6	WDU 16	1.5-25 mm ²	cable end sleeve	2.4
154	WFF 70	2.5-95 mm ²	cable lug M8	12	WDU 35	2.5-50 mm ²	cable end sleeve	4.5
183	WFF 70	2.5-95 mm ²	cable lug M8	12	WDU 35	2.5-50 mm ²	cable end sleeve	4.5
231	WFF 300	25-300 mm ²	cable lug M16	60	WDU 95 N	16-150 mm ²	cable end sleeve	20
291	WFF 300	25-300 mm ²	cable lug M16	60	WDU 95 N	16-150 mm ²	cable end sleeve	20
355	WFF 300	25-300 mm ²	cable lug M16	60	WDU 95 N	16-150 mm ²	cable end sleeve	20
380	WFF 300	25-300 mm ²	cable lug M16	60	WDU 95 N	16-150 mm ²	cable end sleeve	20
436	WFF 300	25-300 mm ²	cable lug M16	60	WDU 95 N	16-150 mm ²	cable end sleeve	20

Table 6.2: 440 - 480 V, 60 Hz

6.2.4 Fuses

In order to protect the installation against electrical and fire hazards, all filters in an installation must be short-circuit and over-current protected according to national/international regulations.

To protect both drive and filter please choose the type of fuses recommended in the VLT^{\circledR} Design Guide. The maximum fuse rating per filter size is listed below.

Filter current		
380 V, 60 Hz	460 V, 60 Hz	
400 V, 50 Hz		Maximum size of fuse
[A]	[A]	[A]
10	10	16
14	14	35
22	19	35
29	25	50
34	31	50
40	36	63
55	48	80
66	60	125
82	73	160
96	95	250
133	118	250
171	154	315
204	183	350
251	231	400
304	291	500
325	355	630
380	380	630
480	436	800

In applications where filters are paralleled it might be necessary to install fuses in front of each filter and in front of the drive.



6.3 Mechanical Dimensions

6.3.1 Sketches

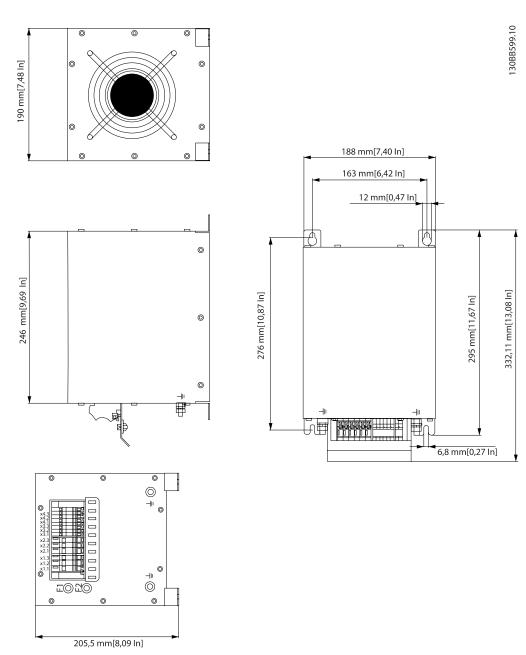


Illustration 6.1: X1 no fan



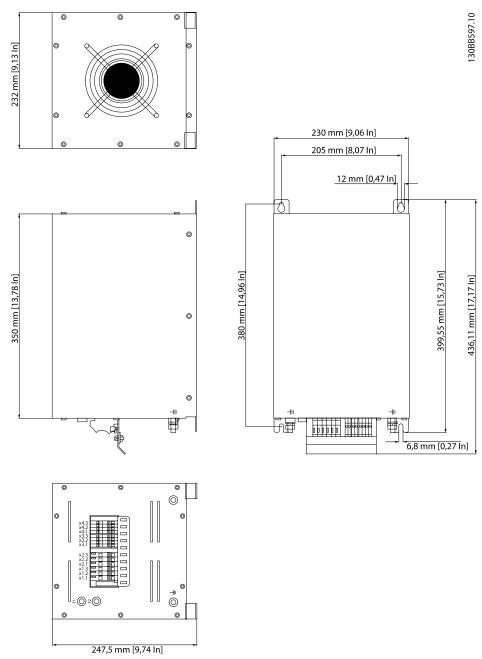


Illustration 6.2: X2 internal fan





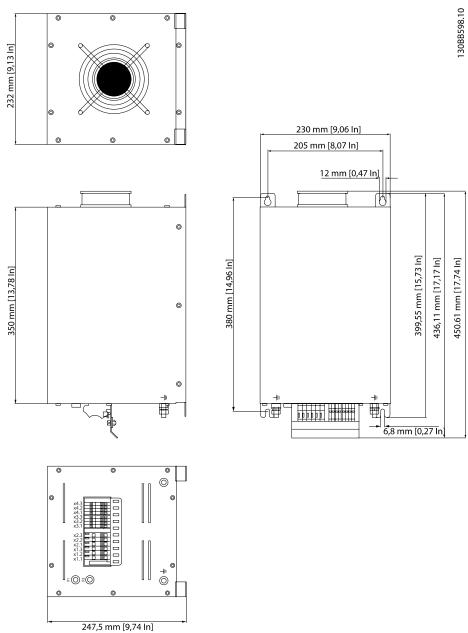


Illustration 6.3: X2 external fan



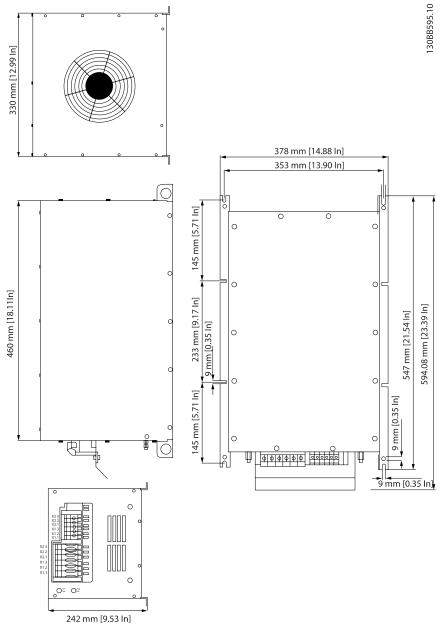


Illustration 6.4: X3 internal fan



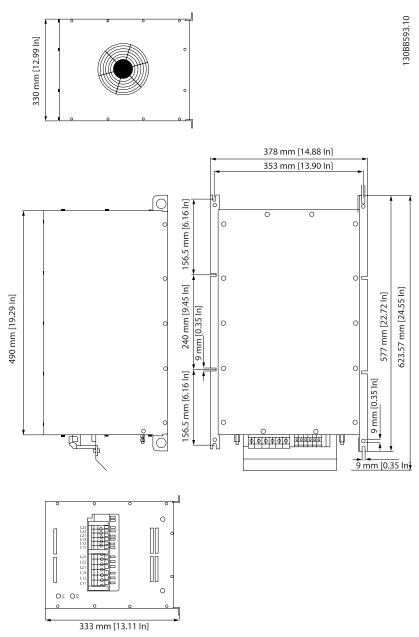


Illustration 6.5: X4 internal fan



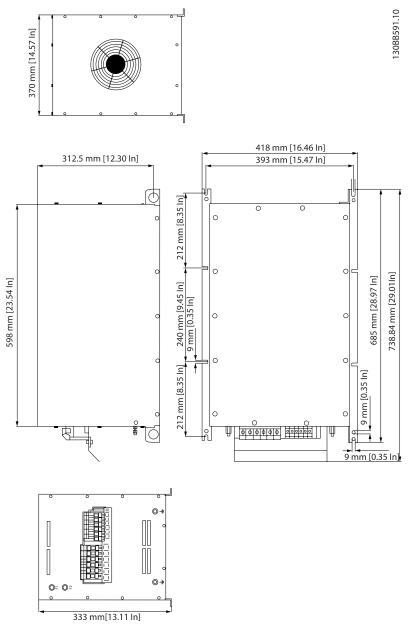


Illustration 6.6: X5 internal fan



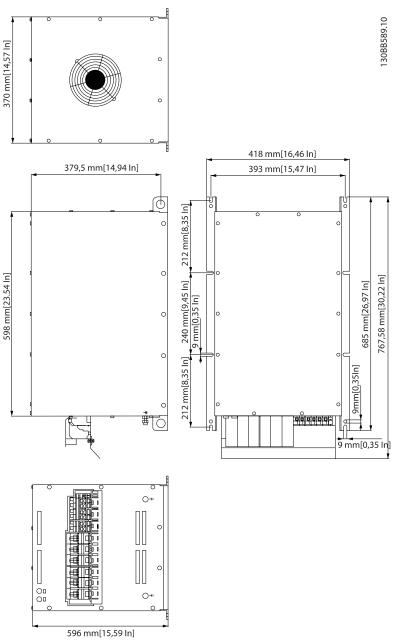


Illustration 6.7: X6 internal fan

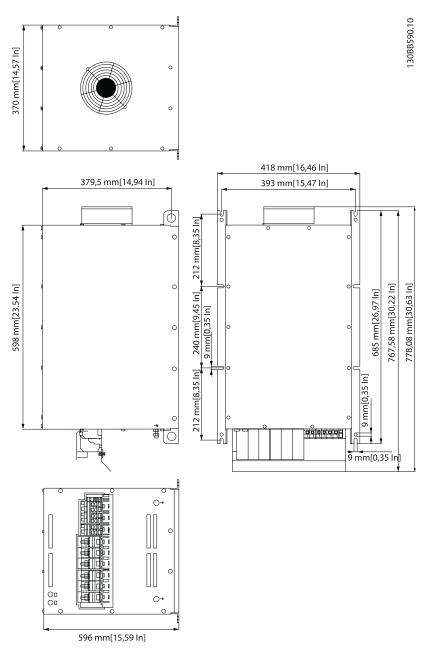


Illustration 6.8: X6 external fan



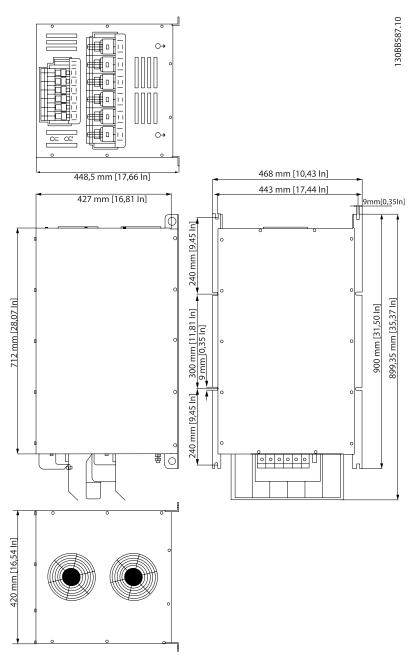


Illustration 6.9: X7 internal fan

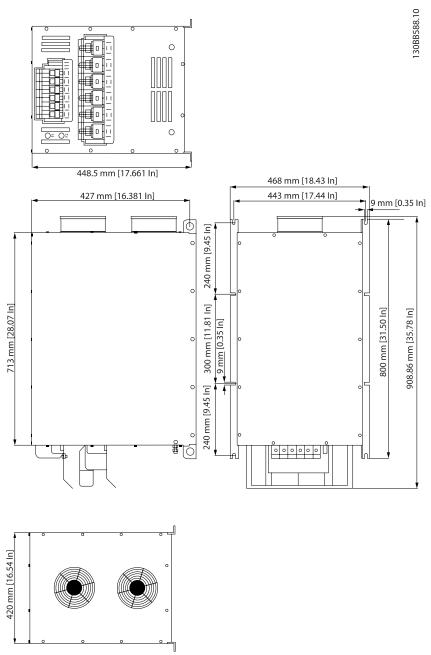


Illustration 6.10: X7 external fan

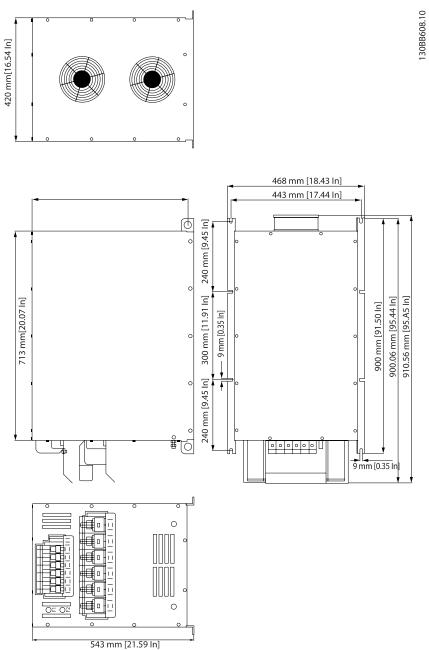


Illustration 6.11: X8 internal fan

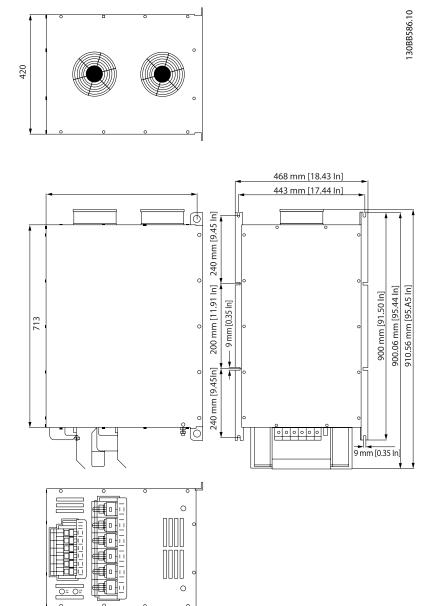


Illustration 6.12: X8 external fan

543 mm [21.53 ln]



6.3.2 Physical Dimension

Enclosure	Dimensions in	Dimensions in mm				
type	A (height)	B (width)	C (Depth)			
X1	245	190	205			
X2	350	230	248			
Х3	460	330	242			
X4	490	330	333			
X5	747	370	333			
X6	778	370	400			
X7	909	468	450			
X8	911	468	550			

6.3.3 Weight

	AHF0	AHF010 380 - 415 V, 50 Hz			0 - 415 V, 50 Hz AHF005 380 - 415 V, 50 Hz		
Current	fram	weight	weight			weight	
rating	e	IP20	IP00	frame	weight IP20	IP00	
[A]	size	[kg]	[kg]	size	[kg]	[kg]	
10	X1	12	8	X1	16	12	
14	X1	13	9	X1	20	16	
22	X2	22	17	X2	34	29	
29	X2	25	20	X2	42	37	
34	Х3	36	30	Х3	50	44	
40	Х3	40	33	Х3	52	45	
55	Х3	42	35	Х3	75	68	
66	X4	52	45	X4	82	75	
82	X4	56	47	X4	96	87	
96	X5	62	52	X5	104	94	
133	X5	74	64	X5	130	120	
171	Х6	85	74	X6	135	124	
204	Х6	105	94	X6	168	157	
251	X7	123	106	X7	197	180	
304	X7	136	120	X7	220	204	
325	X7	142	126	X7	228	212	
381	X7	163	147	X8	260	244	
480	X8	205	186	X8	328	309	

	AHF010 380 - 415 V, 60 Hz			AHF005	380 - 415	V, 60 Hz
Current	4	weight	weight	£	weight	weight
rating	frame	IP20	IP00	frame	IP20	IP00
[A]	size	[kg]	[kg]	size	[kg]	[kg]
10	X1	12	8	X1	16	12
14	X1	13	9	X1	20	16
22	X2	22	17	X2	34	29
29	X2	25	20	X2	42	37
34	Х3	36	30	Х3	50	44
40	Х3	40	33	Х3	52	45
55	Х3	42	35	Х3	75	68
66	X4	52	45	X4	82	75
82	X4	56	47	X4	96	87
96	X5	62	52	X5	104	94
133	X5	74	64	X5	130	120
171	X6	85	74	X6	135	124
204	Х6	105	94	X6	168	157
251	X7	123	106	X7	197	180
304	X7	136	120	X7	220	204
325	X7	142	126	X7	228	212
381	X7	163	147	X8	260	244
480	X8	205	186	X8	328	309

				AHF005 440 - 480 V, 60		
	AHF010 440 - 480 V, 60 Hz			Hz		
Current			weight		weight	weight
rating	frame	weight IP20	IP00	frame	IP20	IP00
[A]	size	[kg]	[kg]	size	[kg]	[kg]
10	X1	12	8	X1	16	12
14	X1	13	9	X1	20	16
19	X2	22	17	X2	34	29
25	X2	25	20	X2	42	37
31	X3	36	30	Х3	50	44
36	Х3	40	33	Х3	52	45
48	Х3	42	35	Х3	75	68
60	X4	52	45	X4	82	75
73	X4	56	47	X4	96	87
95	X5	62	52	X5	104	84
118	X5	74	64	X5	130	120
154	X6	85	74	X6	135	124
183	Х6	105	94	X6	168	157
231	X7	123	106	X7	197	180
291	X7	136	120	X7	220	204
355	X7	163	126	X7	260	212
380	X7	178	147	X8	295	244
436	X8	205	186	X8	328	309

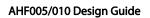


7 How to Programme the Frequency Converter

7.1.1 DC-link Compensation Disabling

The FC series include a feature which ensures that the output voltage is independent of any voltage fluctuation in the DC link, e.g. caused by fast fluctuation in the mains supply voltage. In some cases this very dynamic compensation can produce resonances in the DC link and should then be disabled. Typical cases are where AHF005/010 is used on supply grids with high short circuit ratio. Fluctuations can often be recognized by increased acoustical noise and in extreme cases by unintended tripping. To prevent resonances in the DC-link, it is recommended to disable the dynamic DC-link compensation by setting par. 14-51 to off.

14-51 DC Link Compensation						
Option:		Function:				
[0]	Off	Disables DC Link Compensation.				
[1] *	On	Enables DC Link Compensation.				







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Partial Weighted Harmonic Distortion	
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Power Factor	
R	
Reactive Power	
Real Power	
S	
Screening	2
Short Circuit Ratio	
Т	
The Low-voltage Directive (73/23/eec)	
Total Current Harmonic Distortion	1.
Total Demand Distortion	
Total Harmonic Distortion (thd)	

True Power Factor